

# A High Efficiency Step-Up DC-DC Converter Combining KY and Multilevel Modular Converter with Low Switching Voltage and Current Stress

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**Abstract:** A novel step up converter is presented, which combines the KY converter and the Multilevel Modular Converter (MMC). The proposed system combines KY and MMC. MMC is integrated to reduce the voltage and current stresses of switching device, improve efficiency, and fault-tolerant capability. The KY converter contains SR boost converter and coupled inductor with the turn's ratio it is used to improve the voltage gain. Therefore, the voltage gain is higher in the converter output, and can be determined by adjusting both the duty cycle and the turn's ratio. The proposed step-up converter has no floating output current, and reducing the output voltage ripple. By combining achieves the features of KY and MMC.

## 1. Introduction

Now a days the demand of green power is increased gradually. Solar, wind, fuel, geothermal, biomass are some sources of green power. Lot of applications, converters have much importance, such as boosting the small output voltage to high voltage. The voltage gains of buck-boost converter and traditional boost converter are not high for the loads need. Till now, a lot of voltage-boosting techniques presented, such as inductors and charge pump, coupled inductors, here the output voltage become floating, this will result to increase the complexity of the application, and also these converters are made up of so many components therefore the converters relatively complicated. In many situations the output current are non-pulsating, the voltage gain is inadequate. In HVDC use of DC/DC power converters increase output voltage to the high voltage (HV) level, and it results to efficient transmission for long distances. HVDC results to reduce the power losses, cabling cost, step up grid bulky transformer etc. A new Voltage boosting converter is described here, and combines KY converter with Multilevel Modular Converter. Here KY converter having one SR buck-boost converter connection, and also one coupled inductor having turn's ratio, it is used to increase the voltage gain. The MMC containing SC or CC. SC or CC based

DC-DC converters are used in high power applications and they are having advantages like high power density, high efficiency and control simplicity. For offshore system the exponential voltage gain was implemented using SC DC-DC with the help of Marx concept. Combination of top and bottom cells provide high degree of modularity in each cells. The main important thing of modularity method is, when a single module fails, the converter can function at a reduced power level. It is also practicable to localize any fault in the system, hence system reliability can improve. It's having less maintenance, since it takes small interval of time to clear the fault. In modular structure the usage of cheaper components which is having low voltage / current stress in a system helps to distribute the power handling in multiple modules. MMC is integrated to reduce the voltage and current stresses of switching device, improve efficiency, and fault-tolerant capability.

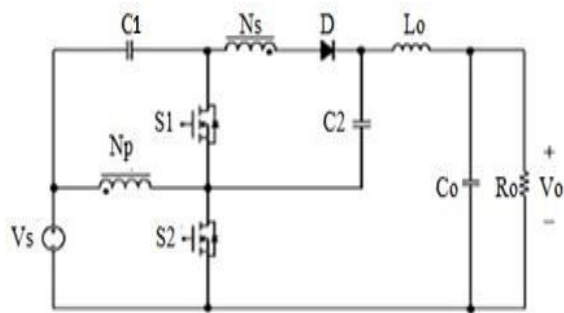
## 2. SYSTEM CONFIGURATIONS

There are two system to be explain, they are,

- 1 KY converter
- 2 Multilevel Modular Converter
- 3 Combination of KY converter and MMC

### 2.1 KY converter

The KY converter is shown in Fig 1, which consists of MOSFETs switches namely  $S_1$  and  $S_2$ , For voltage gain enhancement there uses a coupled inductor with turns ratio, its primary is known as  $N_p$  and the secondary is  $N_s$ ,  $C_1$  is known as energy transferring capacitor,  $C_2$  is charge pump capacitor, A diode  $D_1$  is used, the output side containing Output capacitor  $C_o$ , resistor  $R_o$ , The input voltage is  $V_i$ , output voltage is  $V_o$ .



3. Fig. 1 KY converter

**MODE 1:**

An input voltage  $V_i$  is induced in the primary turns  $N_p$  which causes the  $L_m$  to be magnetized, since the  $S_1$  is turned off and  $S_2$  is turned on, it also causes a voltage which is equivalent to  $V_i * N_s / N_p$  to be induced across the secondary turns  $N_p$ . In addition,  $D_1$  becomes forward biased;  $C_2$  is charged to  $V_i + V_{C1} + V_i * N_s / N_p$  and the voltage across  $L_o$  ie,  $V_{L_o}$  is a negative value, equal to  $V_{C2} - V_o$ , thus making  $L_o$  demagnetised. As a consequence, input voltage  $V_i$  together with the voltage across  $C_1$  ( $V_{C1}$ ), plus the induced voltage on  $N_s$  ( $V_{N_s}$ ), plus the voltage across  $L_o$ , provides the energy to the load. When  $D_1$  become forward biased,  $C_2 = V_i + V_{C1} + V_i * N_s / N_p$ , Voltage across  $L_o = V_{C2} - V_o$ . This voltage will makes the  $L_o$  demagnetised. So in this condition in order to provide the energy to the load, the input voltage together with voltage across  $C_1$ , induced voltage on  $N_s$  and voltage across  $L_o$  add together. Fig. 2 shows the mode 1 operation of KY converter with coupled inductor.

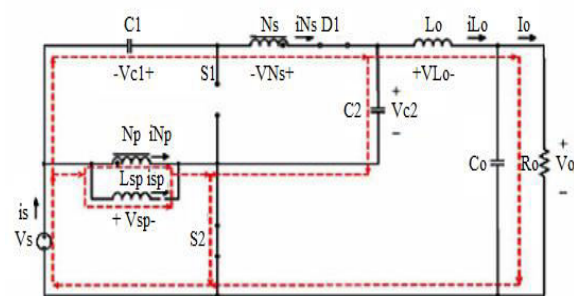


Fig. 2 Mode 1 Operation of KY Converter with Coupled Inductor

**MODE 2:**

$S_1$  is turned on but  $S_2$  is turned off. Therefore, the  $V_{C1}$  voltage is imposed on  $N_p$ , thereby causing the magnetizing inductor  $L_m$  to be demagnetized and the voltage across  $N_s$  to be induced, equal to  $-V_{C1} * N_s / N_p$ . When switch  $S_1$  is on and  $S_2$  is off,  $L_m$  is demagnetised which is caused due to the imposing of voltage  $V_{C1}$  on  $N_p$ . It also causes a voltage to be induced across  $N_s$  which is equal to  $V_{C1} * N_s / N_p$ . Fig. 3 shows the mode 2 operation of KY converter with coupled inductor

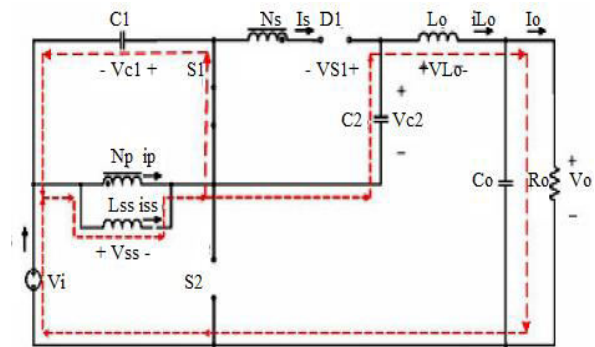


Fig. 3 Mode 2 Operation of KY Converter with Coupled Inductor

When the  $D_1$  become reverse biased.  $L_o$  become magnetised since the voltage on  $L_o$  is equal to  $V_i + V_{C1} + V_{C2} - V_o$  which is a positive value, So energy to the  $l_o$  and load is provided by the addition of input voltage, voltage across  $l_m$  and voltage across  $c_2$ . In addition,  $D_1$  becomes reverse biased, the voltage on  $L_o$  is a positive value, equal to  $V_i + V_{C1} + V_{C2} - V_o$ , thus causing  $L_o$  to be magnetized. As a result, the input voltage  $V_i$ , together with the voltage across  $L_m$  ( $V_{N_p}$ ), plus the voltage across  $C_2$  provides the energy to  $L_o$  and the load. Fig. 3 shows the Mode 2 operation of KY converter with coupled inductor.

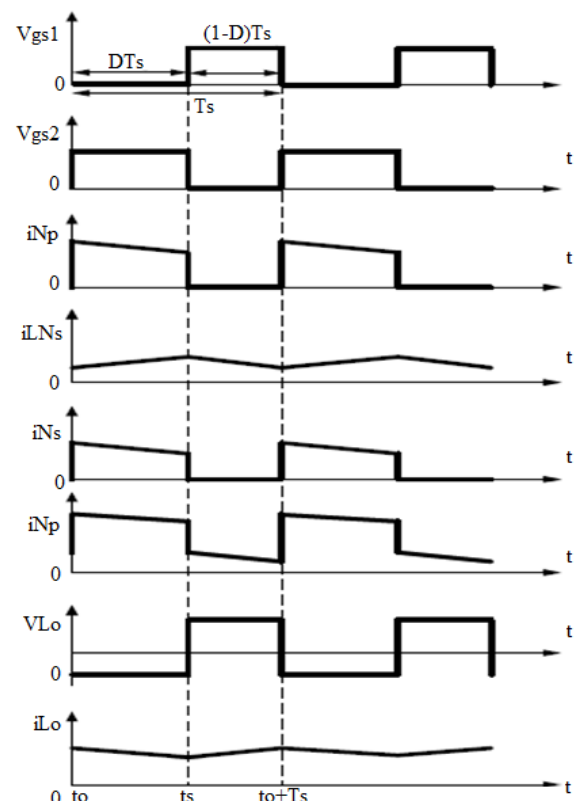


Fig.4 Waveforms of KY Converter

Fig. 4 shows the waveforms of a KY converter with a coupled inductor. Here, the output current is continuous and it is not pulsating. And the output voltage waveform does not contain any ripple.

## 2.2 Multilevel Modular Converter

A five port system is present in SL-based module. This five port system consists of two top and bottom cells, where each one contains 2 capacitors, one inductor and two diodes. The six port DS based module comprised of two cells in the top and bottom of its module and also it has a single active switch one diode, one inductor and one capacitor. The figure is shown below. The input module of the cascaded SL based circuit is integrated to the module #1 which is shown in the figure 5(a), the ports 5 and 6 of module #n of cascaded DS based topology are connected to an output module which has two capacitors and two diodes which is shown in figure 5(b). The below figure shows the above described 2n+1 level cascaded configurations of the SL and DS based modules.

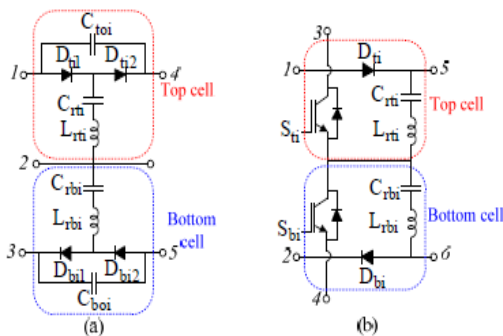


Fig. 5 Structure of SL-Based Module and DS Based Module

## 2.3 Operating Principles of the 2n+1 Level Cascaded SL-and DS-based Configurations

Figures 6 and 7 show the 2n+1 level cascaded SL- and DS-based topologies, respectively. Note that n is an even number in figure 7.

### 2.3.1 Cascaded SL-based Configuration

#### ➤ State I

When  $t_0$  to  $t_1$ ,  $S_b$  is ON ie, the bottom switch, Then  $S_t$  is OFF. The diodes  $D_{ti}$ 's ( $i=1, 2, \dots, n$ ) in each top cell are forward-biased by  $V_s$  and  $C_{toi}$ 's. As a result,  $C_{rti}$ 's are charged by  $V_s$  and  $C_{toi}$ 's ( $i=1, 2, \dots, n-1$ ), as shown in below Figure 3.6(a).

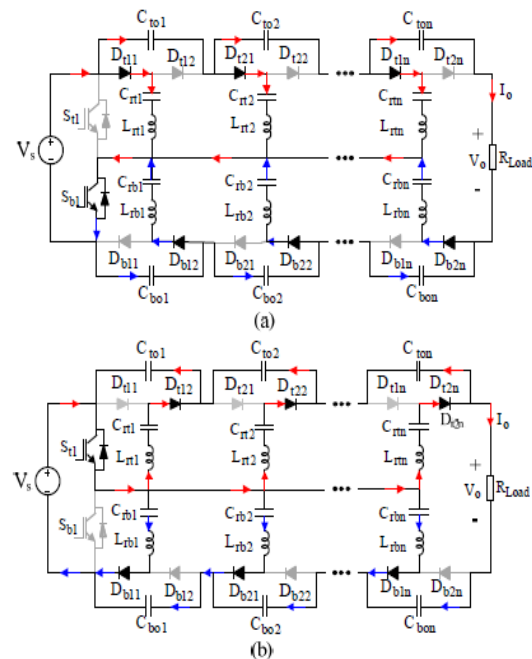


Fig. 6 State I and State III Operation of the 2n+1 Level Cascaded SL-Based Topology.

Here  $C_{ton}$  is discharged to the load. In contrast, in the bottom cells,  $C_{rbi}$ 's are discharged to the output capacitors,  $C_{boi}$ 's. For the general 2n+1 level cascaded SL-based topology, the currents through the top and bottom capacitors are

$$i_{C_{rti}}(t) = \frac{\pi P_o}{V_o} \sin(\omega_r t), i = 1, 2, \dots, n$$

$$i_{C_{rbi}}(t) = -\frac{\pi P_o}{V_o} \sin(\omega_r t), i = 1, 2, \dots, n$$

The voltages of the top and bottom resonant capacitors can be obtained as follows:

$$v_{C_{rti}}(t) = iV_s - \frac{\pi P_o}{V_o C_{rti} \omega_r} \cos(\omega_r t), i = 1, 2, \dots, n$$

$$v_{C_{rbi}}(t) = iV_s + \frac{\pi P_o}{V_o C_{rbi} \omega_r} \cos(\omega_r t), i = 1, 2, \dots, n$$

#### ➤ State II

In this state, all the switches are turned OFF. The diodes are reversed-biased and the resonances stop. Therefore, the inductor currents become zero.

#### ➤ State III

State III begins when  $S_t$  in ON-state and  $S_b$  in OFF-state at  $t_0$ . The diodes  $D_{ti2}$ s and diodes  $D_{bi1}$ s are forward-biased, it is shown figure 3.6(b). In the bottom cells,  $C_{rbi}$ 's are charged by  $V_s$  and  $C_{boi}$ 's ( $i=1, 2, \dots, n-1$ ), whereas  $C_{rti}$ 's are discharged to  $C_{toi}$ 's. As a result, the voltages of  $C_{rbi}$ 's are equal to  $i$  times the input voltage level.

#### ➤ State IV

The operation of this state is similar to that of State II

### 2.3.2 Cascaded DS-based Configuration

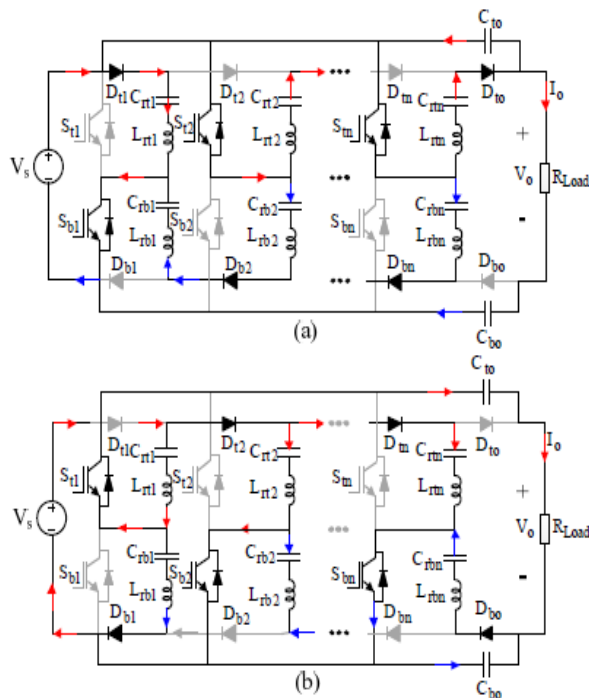


Fig. 7 State I and State III Operation of the 2n+1 Level Cascaded DS-Based Topology

➤ **State I**

At  $t = t_0$ ,  $S_{bi}$  ( $i=1, 3, \dots, n-1$ ) and  $S_{ti}$  ( $i=2, 4, \dots, n$ ) are turned ON, whereas  $S_{bi}$  ( $i=even$ ) and  $S_{ti}$  ( $i=odd$ ) are OFF in the top and bottom cells. Therefore, in the top and bottom cells, the odd numbered  $C_{rti}$ 's and even numbered  $C_{rbi}$ 's are charged by  $V_s$ ,  $C_{rti}$ 's ( $i=2, 4, \dots, n$ ), and  $C_{rbi}$ 's ( $i=1, 3, \dots, n-1$ ). In this state, the output capacitor  $C_{to}$  is charged by  $C_{rn}$ , whereas  $C_{bo}$  is discharged to the load, as shown in figure 3.7(a).

➤ **State III**

During this time interval,  $S_{bi}$ 's ( $i=1, 3, \dots, n-1$ ) and  $S_{ti}$ 's ( $i=2, 4, \dots, n$ ) are OFF, whereas  $S_{bi}$ 's (for  $i$  even) and  $S_{ti}$ 's (for  $i$  odd) are ON. Therefore, in the top cells,  $C_{rti}$ 's ( $i=1, 3, \dots, n-1$ ) are discharged to  $C_{rti}$ 's ( $i=2, 4, \dots, n$ ). The odd numbered  $C_{rbi}$ 's are charged by  $V_s$  and the even numbered  $C_{rbi}$ 's. Figure 8 shows the key voltage and current waveform of MMC.

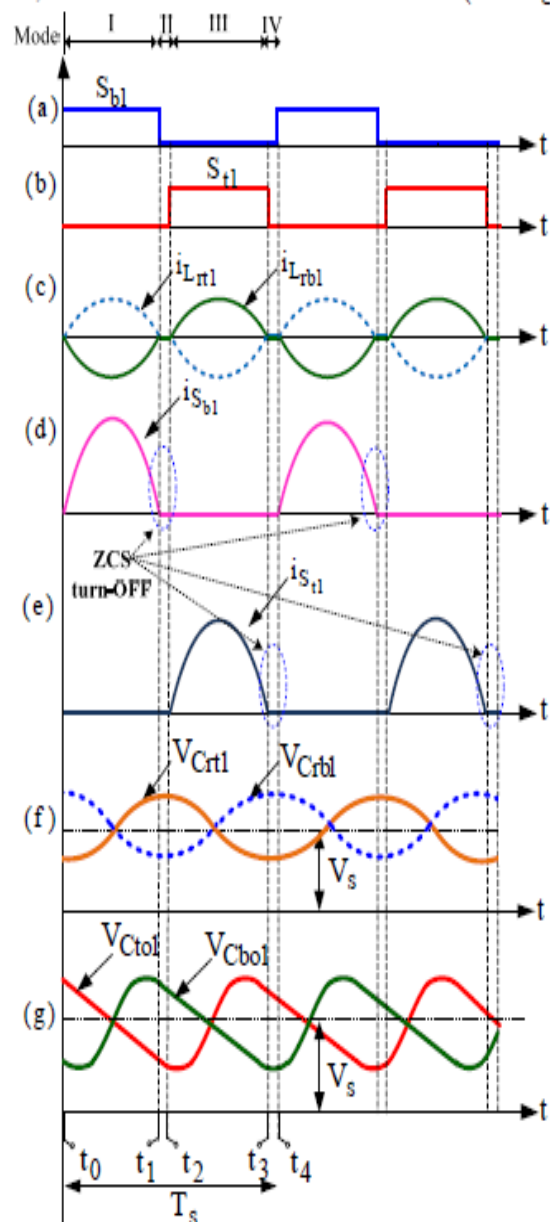


Fig. 8 Key Current and Voltage Waveforms of the MMC

**3. COMBINATION OF KY CONVERTER AND MMC**

Here combining KY converter and Multilevel Modular Converter. The KY converter contains SR boost converter and coupled inductor with the turn's ratio it is used to improve the voltage gain. Therefore, the voltage gain is higher in the converter output, and can be determined by adjusting both the duty cycle and the turn's ratio. The proposed step-up converter has no floating output current, and reducing the output voltage ripple.

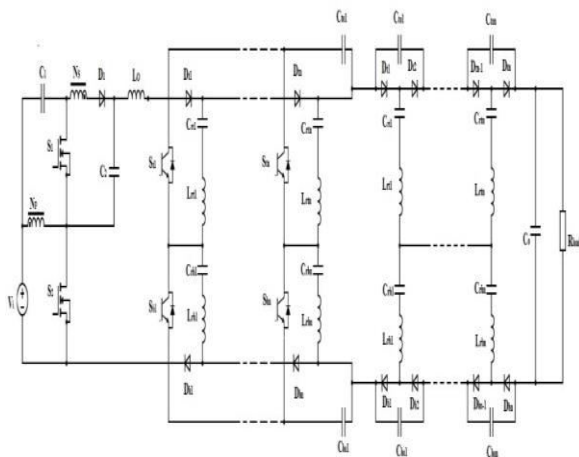


Fig. 9 KY- MMC Converter

The operation of combined configuration is similar individual operation of KY and MMC

### 3.1 Simulation

The simulation is done by using Matlab R2016a Simulink, the specifications and parameters are listed in the table I and II given below.

### 3.2 Simulation Diagram

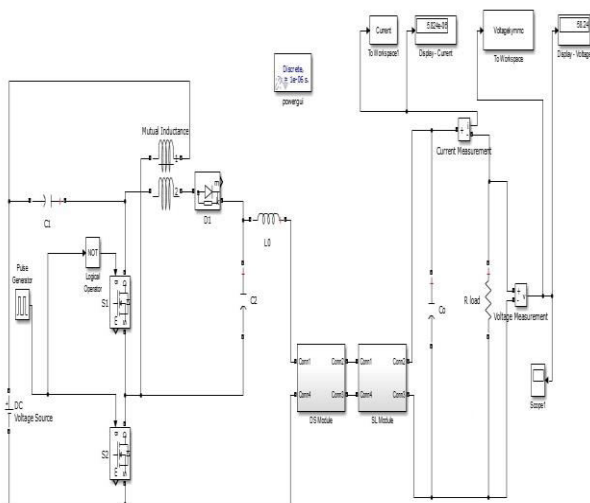


Fig. 10 Simulation Diagram

### 3.2 Simulation Result

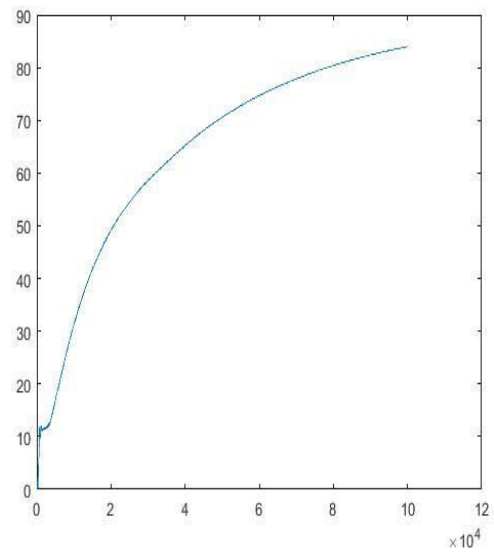


Fig. 11 Simulation Result – Voltage Waveform

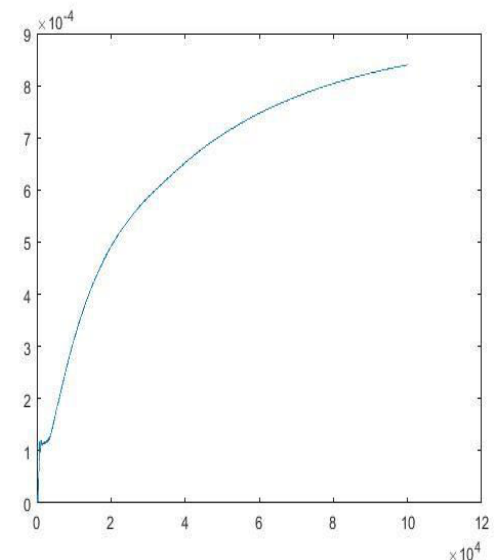


Fig. 11 Simulation Result – Current Waveform

**Table I Five-Level System Specification**

| Specifications              | Value     |
|-----------------------------|-----------|
| Output power                | 0.07056 W |
| Input voltage               | 12 V      |
| Output voltage              | 84 V      |
| Switching frequency for MMC | 4.5 kHz   |
| Switching frequency for     | 100kHz    |

| Parameter                             | Value  |
|---------------------------------------|--|
| KY MOSFET switches $S1, S2$           | STP120NF, $V_{DS}=100V$ , $I_D=120A$ , $R_{on}=10.5m\Omega$                        |
| KY Diode $D1$                         | V20120C, $V_R=120V$ , $I_F(AV)=20A$ , $V_F=0.54V$ @ $I_F=5A$                       |
| KY Energy-transferring capacitor $C1$ | Two 470 $\mu$ F/50V Rubycon capacitors with positive terminals connected in series |
| KY Charge pump capacitor $C2$         | Two 47 $\mu$ F/100V MIEC capacitors connected in parallel                          |
| KY Output capacitor $C_o$             | Two 220 $\mu$ F/100V MIEC capacitors connected in parallel                         |
| KY Coupled inductor Core              | PTS40/27/I 3C92, $N_p:N_s=1:3$ , $L_m=148.7\mu H$ , $L_{l1}=0.3\mu H$ , $k=0.997$  |
| KY Output inductor $L_o$ Core         | ER40/20/13, $N=20$ , air-gap of 0.35mm, $L_o=188\mu H$                             |
| MMC Resonant inductor                 | 2.4 $\mu$ H with powder core   |
| MMC Resonant capacitor                | 6 $\mu$ F/450 V – Film capacitor   |
| MMC Output capacitor                  | 30 $\mu$ F/450 V – Film capacitor  |
| MMC IGBT module                       | 600 V-SKM200GB063D from SEMIKRON   |
| MMC Diode                             | DSEP2X91-06A   |

**Table II Prototype Components**

### 3. CONCLUSION

A multilevel converter is build up with KY converter. In order to improve the voltage gain of the multilevel converter, the KY converter has one coupled inductor which has turns ratio and also it contains a buck boost converter which is rectified

synchronously. In order to reduce the output voltage ripple, the step p converter has no floating output current. The voltage gain is higher in the converter output. And this voltage gain can be find by adjusting its turn's ratio and duty cycle. The MMC consist of SL and DS based modules to achieve the voltage gain and high efficiency. The cascaded DS based topology has many modules and equal power sharing is achieved among its modules. Due to this, the switching devices experiences low losses and low cost than other approaches. By looking the power device count, efficiency and fault tolerant capability, the cascaded hybrid topology is really advantage than other DC to DC approaches. When external fault is added to the circuit, the circuit remains stable. Hence the system remains highly fault tolerant.

### 4. ACKNOWLEDGEMENT

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### 5. REFERENCES

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